



MARITIME TECHNOLOGY

A NEW APPROACH TO SPRING/DAMPER SYSTEMS IN SUSPENSION SEATS

Edgar Schmidtke, WTD 71, DEU

(unclassified)



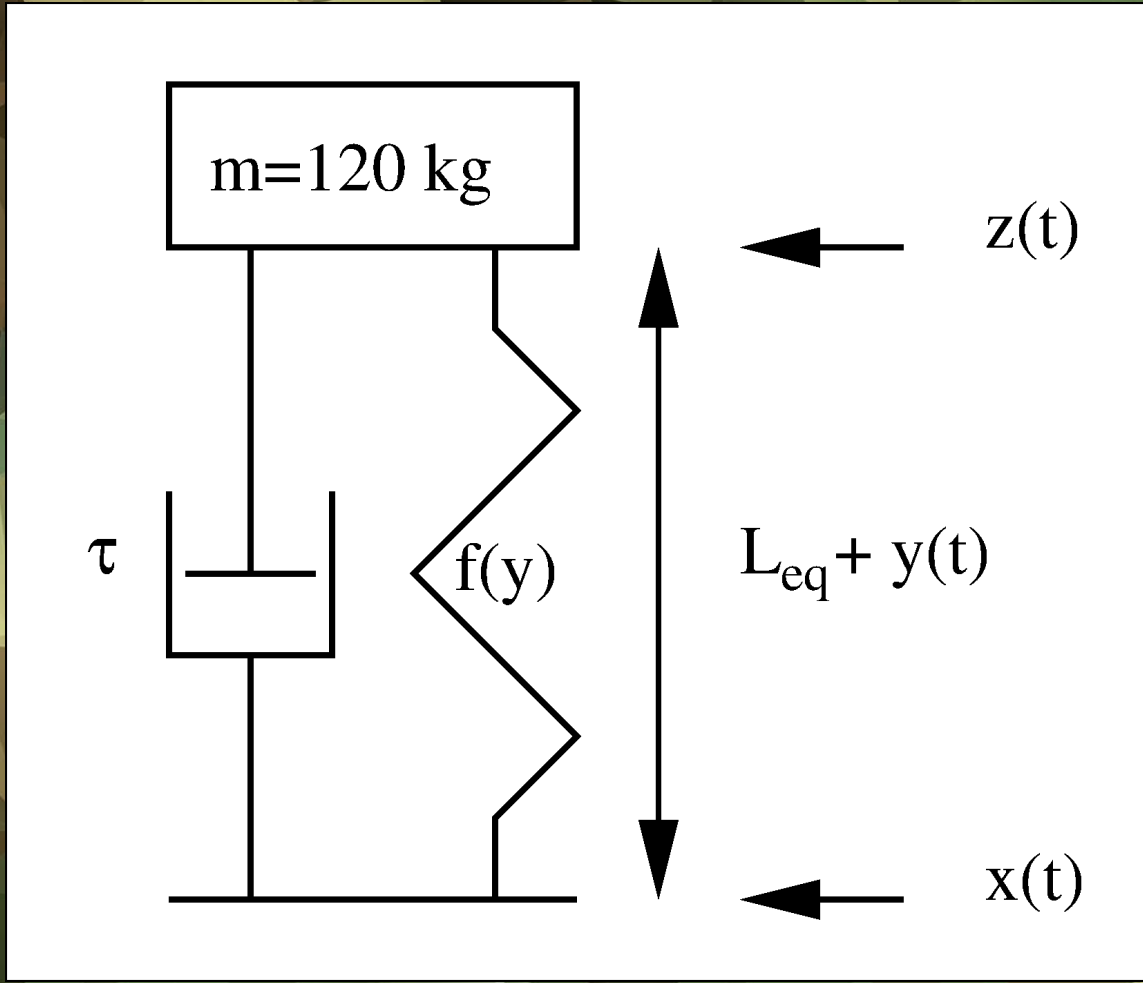
BUNDESWEHR

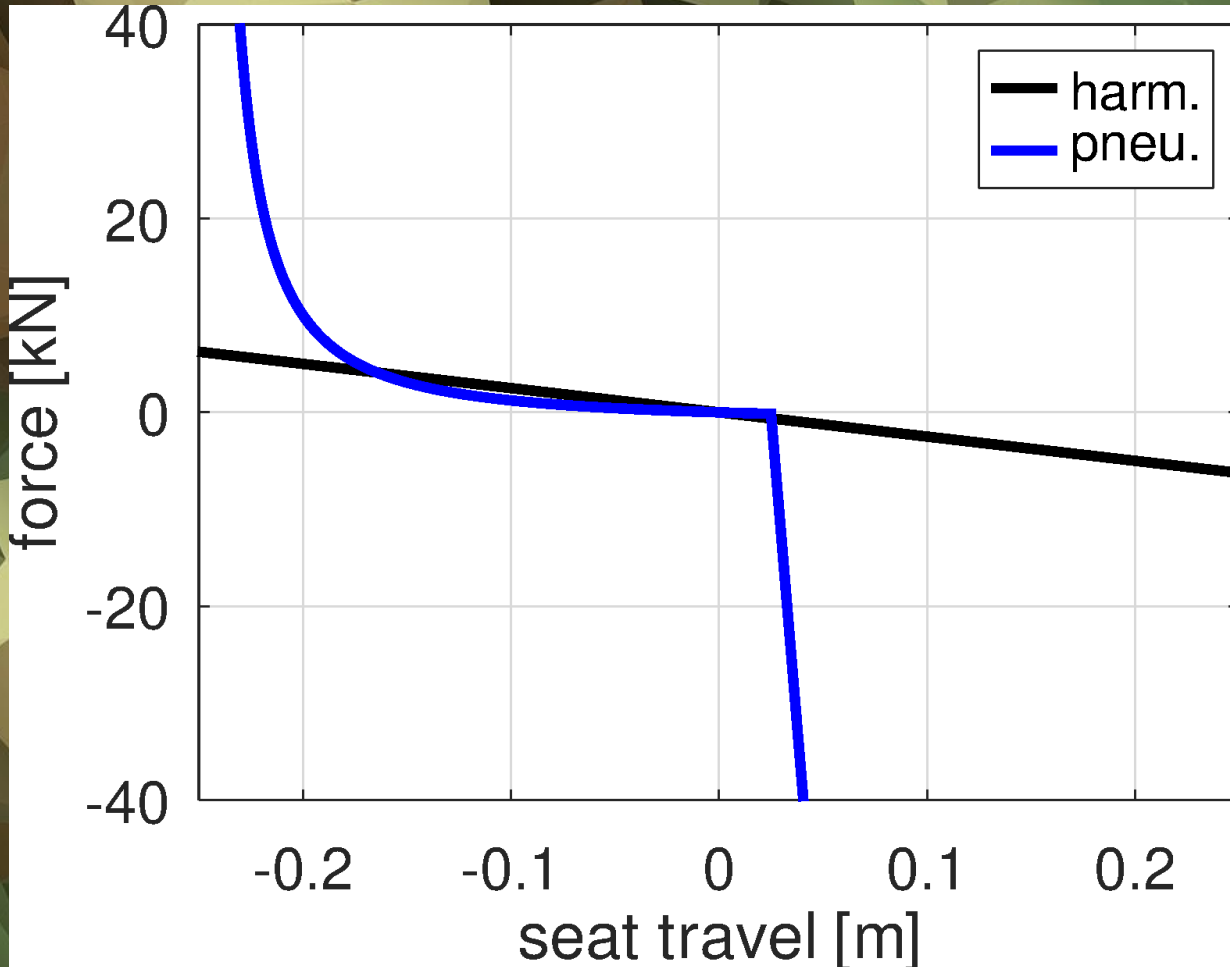
1. Introduction
2. Theory
3. Experimental Data
4. Limits and §§
5. New approach to get 3. closer to 4.

Introduction

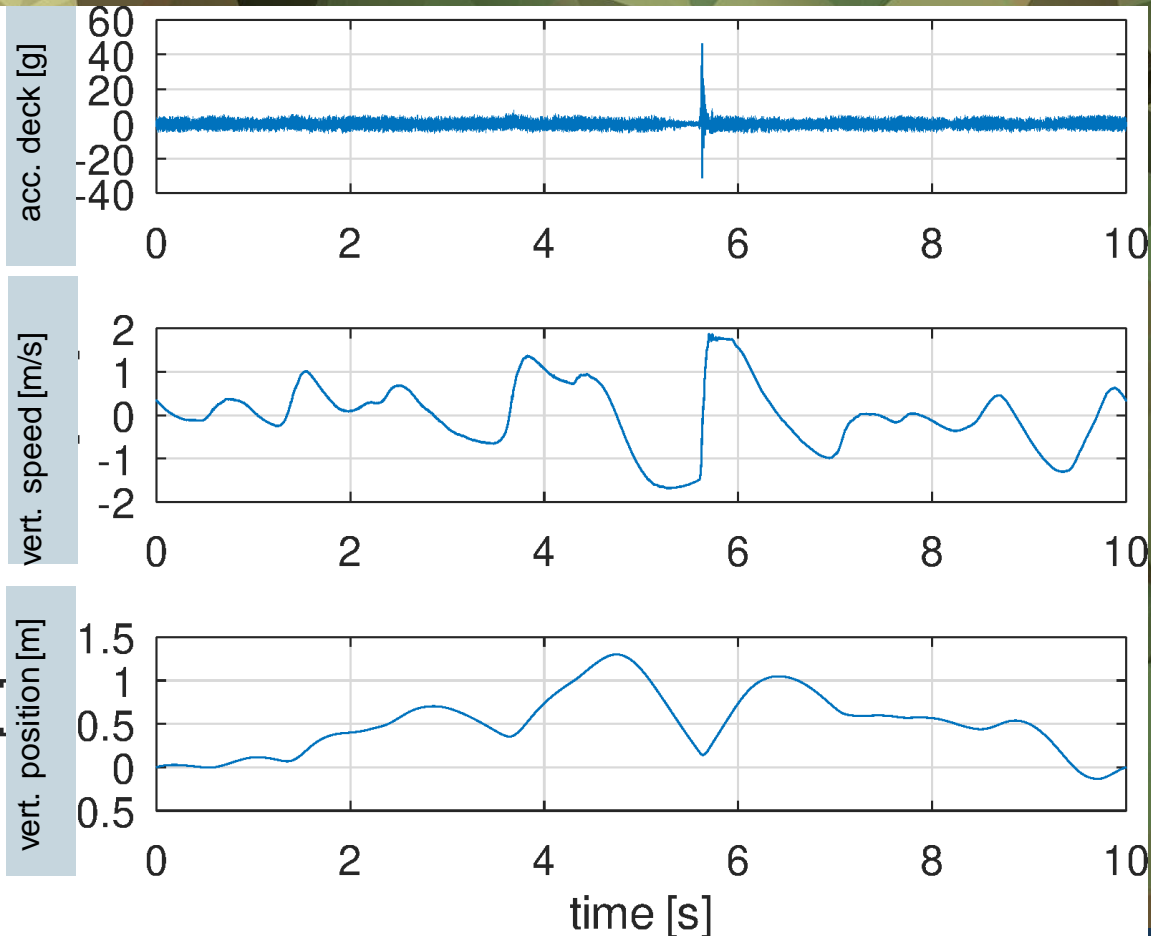
- WTD 71 = Bundeswehr Technical Center for Ships, Naval Weapons, Maritime Technology and Research
 - € Federal Office of Bundeswehr Equipment, Information Technology and In-Service Support (BAAINBw)
 - € DEU MoD
- Section 310 = Shipbuilding Technology, Equipment
- Section 340 = Shock and Vibration Center

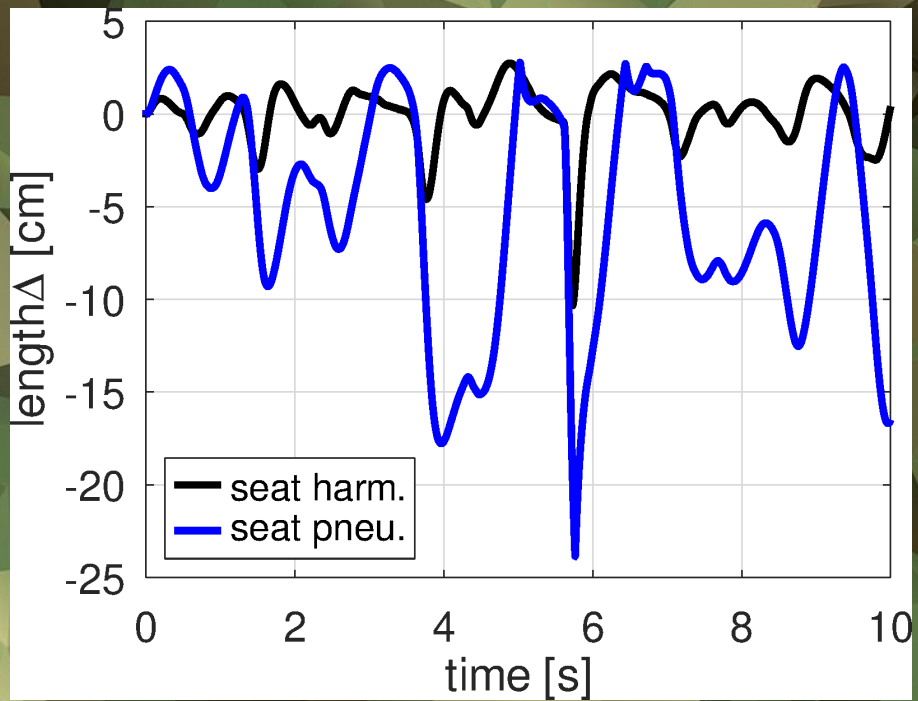
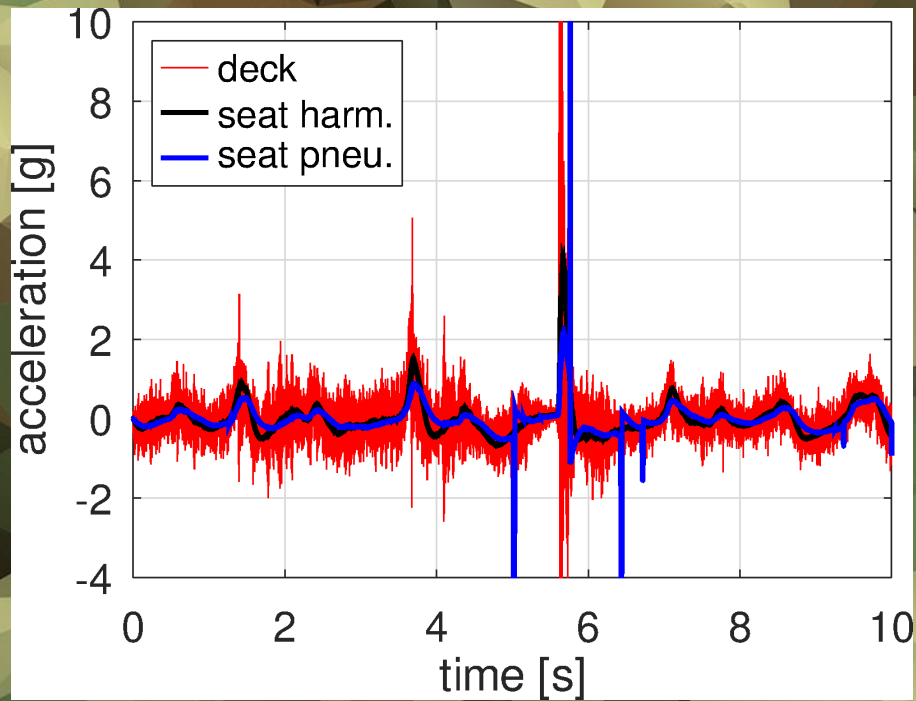






- near Helgoland, North Sea
- 4 Bft
- SOG 24 kn
- Wave height 1,0 m – 1,5 m
- Sea state 3
- BUSTER boat, RHIB 10 m
- middle (of 3) seat
- deck acceleration
- raw data





$$\text{DEU §§ : } A(T) = \sqrt{\frac{1}{T} \cdot \int_0^T a_{wz}^2(t) dt} ; \quad A(8h) \leq 0.8 \text{ m/s}^2$$

$$\Rightarrow T \leq 8h \cdot \left(\frac{0.8 \text{ m/s}^2}{A(T)} \right)^2$$

$$\text{DRI : } \ddot{z}(t) = \ddot{\delta}(t) + 2\varepsilon\omega \cdot \dot{\delta}(t) + \omega^2 \cdot \delta(t) ; \quad \varepsilon = 0.224 , \quad \omega = 52.9 \text{ rad/s}$$

upwards, compression of spine : $\max\{\delta(t)\} \leq \begin{cases} 53.3 \text{ mm} & \text{Training} \\ 63.3 \text{ mm} & \text{Emergency} \end{cases}$

- DEU §§: Lärm- und Vibrationsarbeitsschutzverordnung (decree for the protection of personel against noise and vibration at work)
- DRI, Dynamic Response Index, see
 - Maritime Safety Commitee Resolution: „Testing of Life-Saving Appliances“
 - NATO Standard AEP-55: „Procedures For Evaluating The Protection Level of Armoured Vehicles - IED Threat“

deck: $A_{wz}(10\text{ s}) = 3.45\text{ m/s}^2$, $T \sim 26\text{ min}$
harm.: $A_{wz}(10\text{ s}) = 2.91\text{ m/s}^2$, $T \sim 36\text{ min}$
pneum.: $A_{wz}(10\text{ s}) = 4.78\text{ m/s}^2$, $T \sim 13\text{ min}$ (hard stops!)

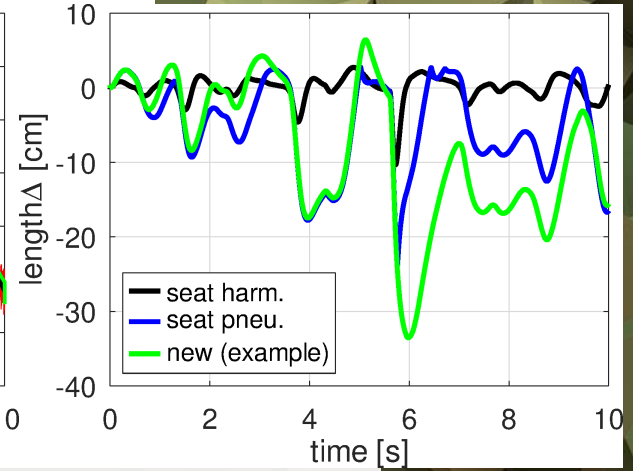
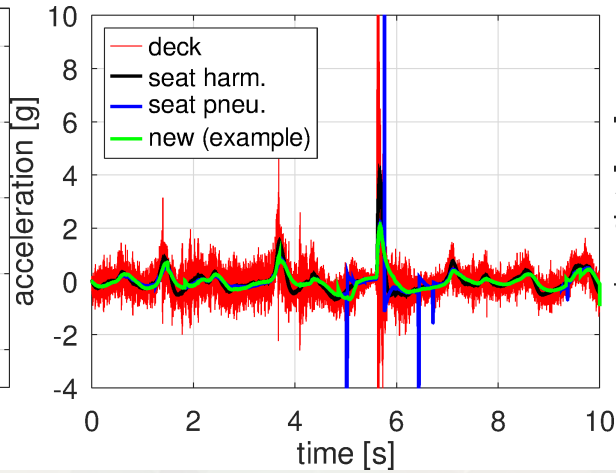
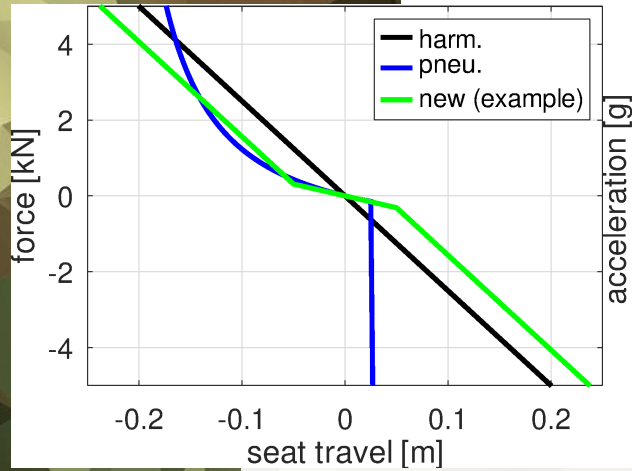
deck: $A_{wz}(2\text{ s}) = 1.42\text{ m/s}^2$, $T \sim 152\text{ min}$
harm.: $A_{wz}(2\text{ s}) = 1.62\text{ m/s}^2$, $T \sim 118\text{ min}$ (excitation close to f_0)
pneum.: $A_{wz}(2\text{ s}) = 0.98\text{ m/s}^2$, $T \sim 320\text{ min}$

deck: $\delta_{\max}(10\text{ s}) = 25.8\text{ mm}$
harm.: $\delta_{\max}(10\text{ s}) = 18.4\text{ mm}$
pneum.: $\delta_{\max}(10\text{ s}) = 28.2\text{ mm}$

δ_{\max} seems not to be critical.

1. Use soft/weak/long springs
2. Avoid hard stops

Define Spring characteristic



deck: $A_{wz}(10\text{ s}) = 3.45\text{ m/s}^2$, $T \sim 26\text{ min}$
harm.: $A_{wz}(10\text{ s}) = 2.91\text{ m/s}^2$, $T \sim 36\text{ min}$
pneum.: $A_{wz}(10\text{ s}) = 4.78\text{ m/s}^2$, $T \sim 13\text{ min}$ (hard stops!)
new: $A_{wz}(10\text{ s}) = 1.73\text{ m/s}^2$, $T \sim 103\text{ min}$

deck: $\delta_{\max}(10\text{ s}) = 25.8\text{ mm}$
harm.: $\delta_{\max}(10\text{ s}) = 18.4\text{ mm}$
pneum.: $\delta_{\max}(10\text{ s}) = 28.2\text{ mm}$
new: $\delta_{\max}(10\text{ s}) = 9.4\text{ mm}$

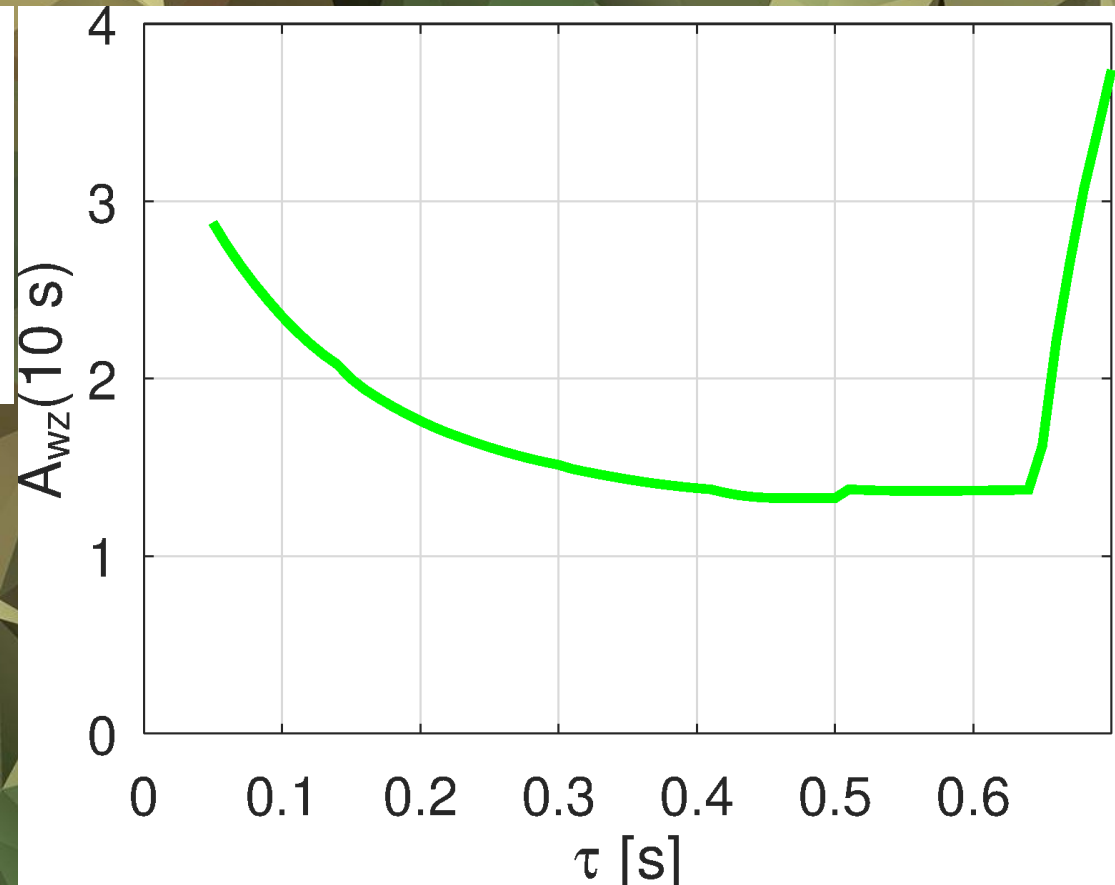
$\tau = 0.21\text{ s}$

Optimize τ

new: $A_{wz}(10\text{ s}) = 1.73\text{ m/s}^2$
 $T \sim 103\text{ min}$, $\tau = 0.21\text{ s}$

new_{opt}: $A_{wz}(10\text{ s}) = 1.33\text{ m/s}^2$
 $T \sim 174\text{ min}$, $\tau = 0.49\text{ s}$

new: $\delta_{\max}(10\text{ s}) = 9.4\text{ mm}$
new_{opt}: $\delta_{\max}(10\text{ s}) = 5.3\text{ mm}$



Conclusion and way ahead

- Spring should work in + and – direction (avoid hard stops)
- **Combine spring and damper in a single material.**
 - National study (2023) about rubber materials
 - select caoutchouc
 - design form
 - optimize τ (τ variable?, electro-rheologic?)
- Be aware of heating/cooling ($P \sim$ some 10 W)
- Use „standard“ (t.b.d.) time signal.

Thank you for your attention

Spare 1

equation of motion : $-\ddot{x} = \ddot{y} + \frac{2}{\tau} \cdot \dot{y} + f(y)$; $z = x + L_{eq} + y$

harm. osc. : $f(y) = -\omega_0^2 \cdot y$

$$\omega_0 = \sqrt{\kappa/m}, \quad \kappa = 25 \text{ kN/m}$$

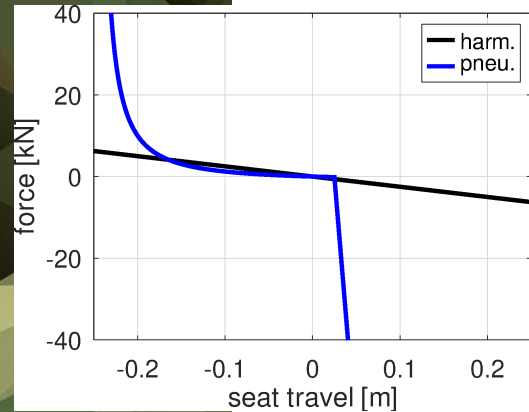
Eigenfrequency $f_{0,harm.} \simeq 2.3 \text{ Hz}$

pneum. (one sided) : $f(y) = g \cdot \left(\frac{1}{\left(1 + \frac{y}{L_{eq}}\right)^\gamma} - 1 \right)$; $g = 9.81 \text{ m/s}^2$

$$L_{eq} = 25 \text{ cm} ; \quad \gamma = c_p/c_v \simeq 1.4 \text{ (air)}$$

$$y \ll L_{eq} \Rightarrow f(y) \simeq - \underbrace{\frac{g \cdot \gamma}{L_{eq}}}_{\omega_{0,pneum.}^2} \cdot y$$

Eigenfrequency $f_{0,pneum.} \simeq 1.2 \text{ Hz}$



both : $\tau := 1.5/\omega_0$

$\ddot{z}(t)$ must not be confused with measurements according to EN 30326-1

mean heating power $\langle P \rangle$

$$\langle P \rangle = \frac{2 \cdot m}{\tau \cdot T} \int_0^T |\dot{y}(t)|^2 dt$$

τ needed for calculation!

$$\frac{y_0}{x_0} = \frac{\varepsilon^2}{\sqrt{(1 - \varepsilon^2)^2 + (\varepsilon/\varepsilon_0)^2}}$$
$$\varepsilon = \Omega/\omega_0$$
$$\varepsilon_0 = \omega_0\tau/2$$
$$\implies \tau = \frac{2}{\omega_0 \cdot \varepsilon} \cdot \frac{1}{\sqrt{(x_0/y_0)^2 - (1 - (1/\varepsilon)^2)^2}}$$

Helgoland data set: $\langle P \rangle \sim 65 \text{ W}$

$$P = P_{em} + P_{conv.} + P_d$$

em: electro magnetic (radiation)

conv.: free convection

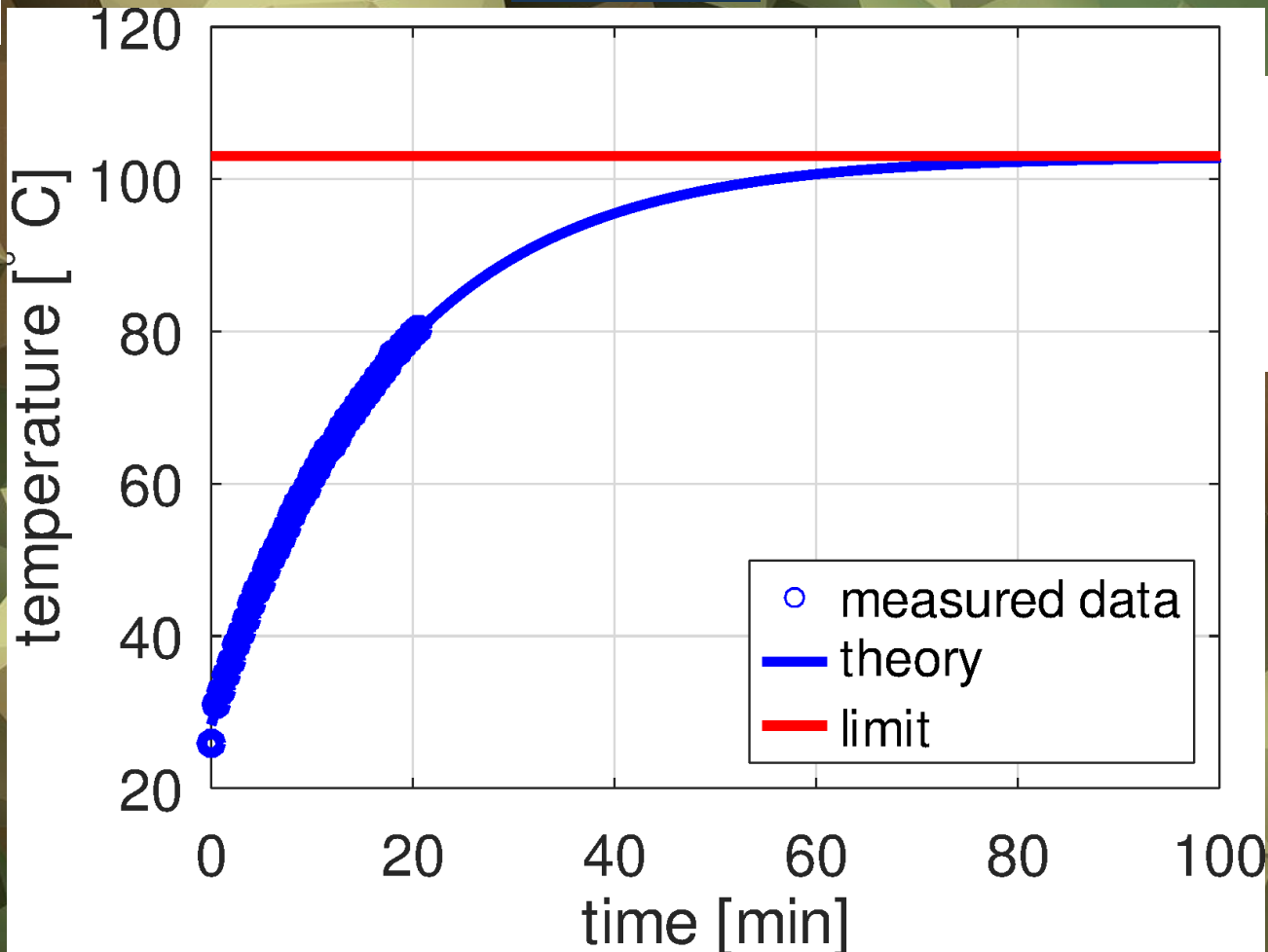
d: dissipation (heating the damper)

Ignoring higher orders of rescaled temperature $[(T-T_{air})/T_{air}]$ in radiation terms: $[\]^2$ $[\]^3$ $[\]^4$

$$T = T_{air} + \delta T \cdot \left(1 - e^{-t/\tau_T}\right)$$

Spare 4

WTD 71



6 Hz

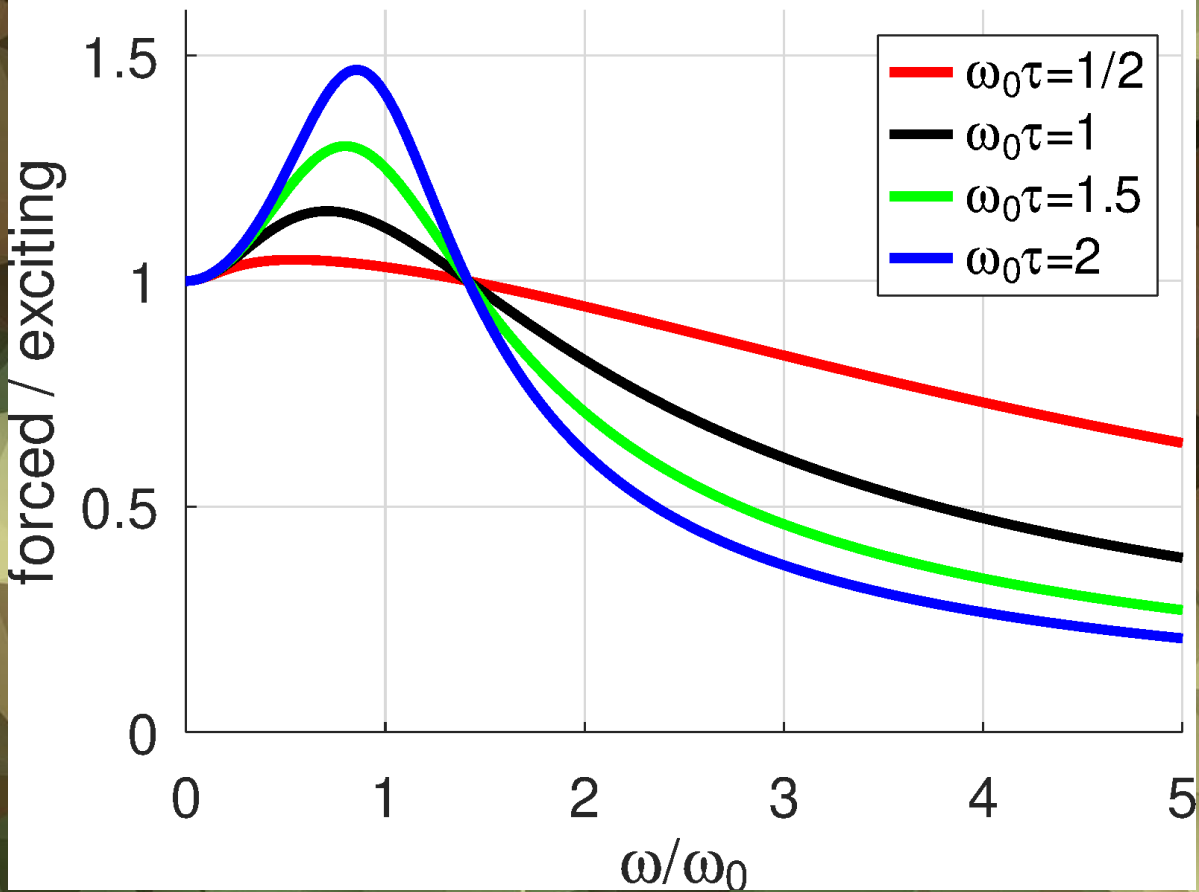
$x_0=15$ mm
(peak2peak)

$$P_{eq.} = \frac{T - T_{air}}{T_{air}} \cdot 267 \text{ W}$$

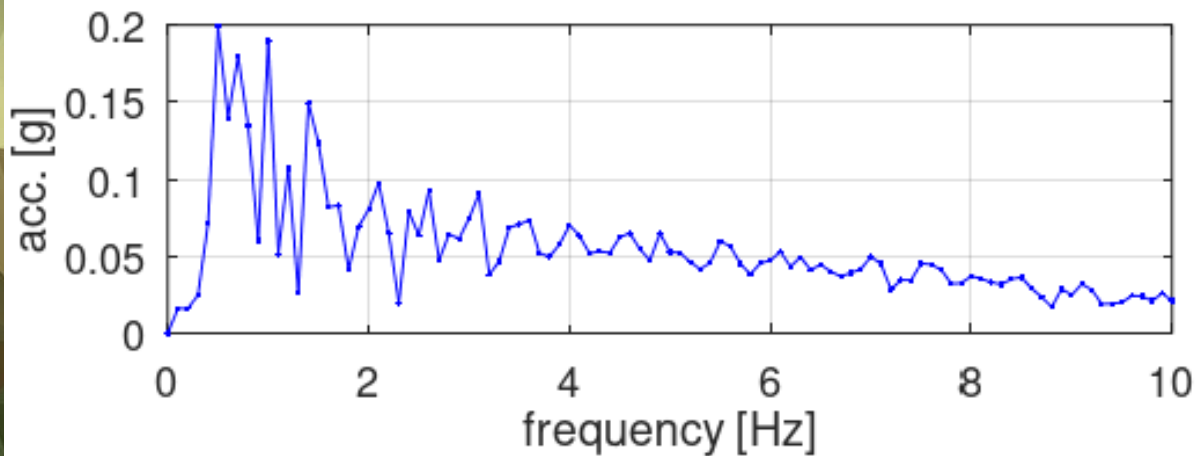
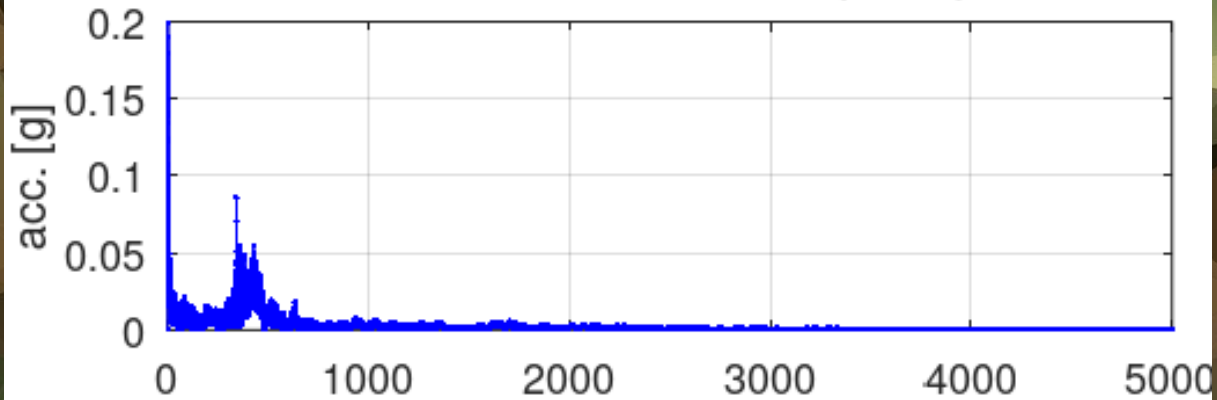
$$T_{air} = \text{(absolute) air Temperature [K]}$$

- * Cooling mechanisms: Radiation and free convection, no forced convection (i.e. cooling air flow)
- * P_{eq} = heating power, that leads to equilibrium temperature T_{eq}
- * Model damper is a cylinder
 - $L_{eq} = 25 \text{ cm}$
 - Diameter 5 cm
- * $T_{air} \sim 300 \text{ K}$

ratio of amplitudes

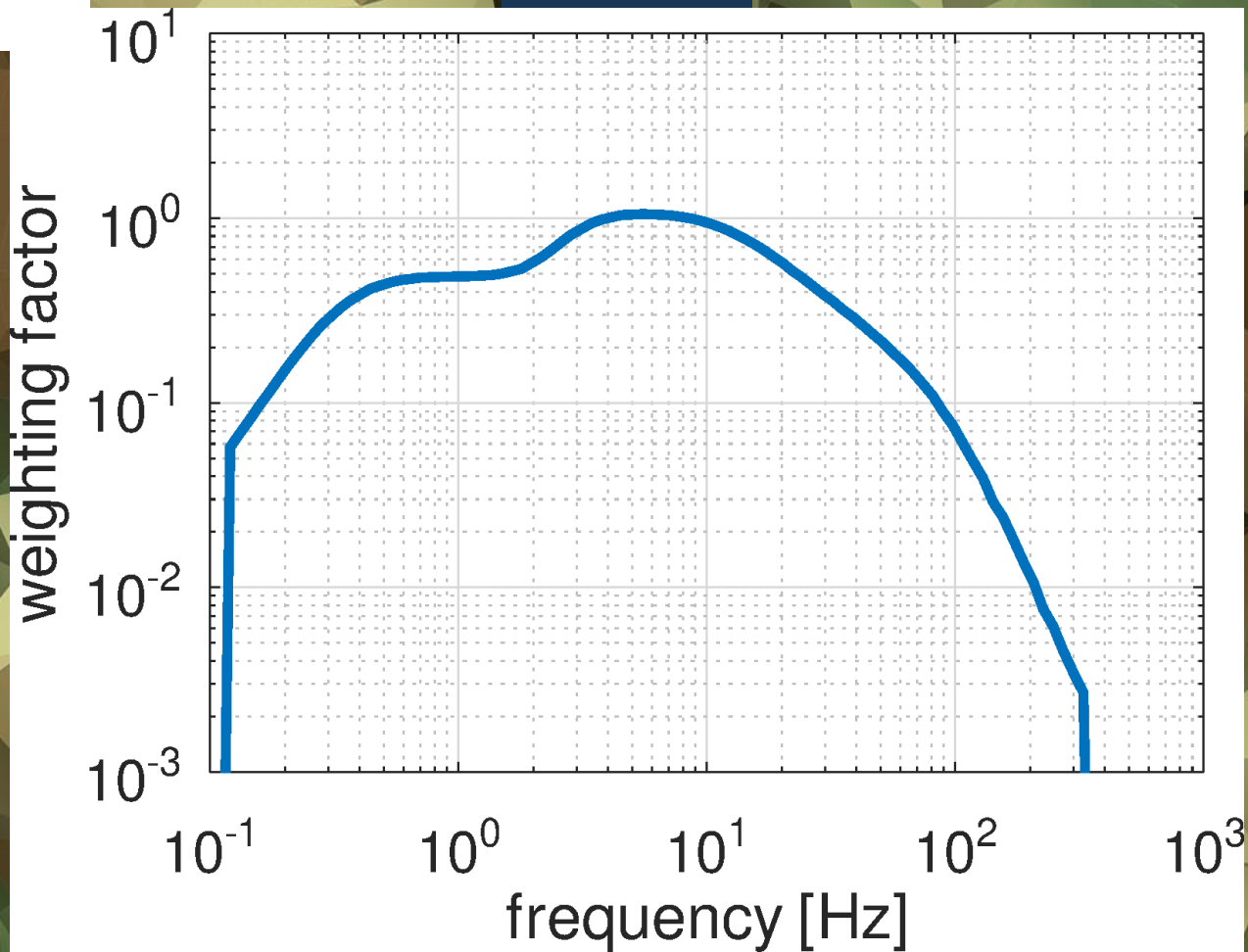


vertical acceleration (deck)



Spare 7

WTD 71



Spare 8

WTD 71

